

AGMA 901-A92

(Reaffirmed March 10, 2015)

AGMA Information Sheet

A Rational Procedure for the Preliminary Design of Minimum Volume Gears American Gear A Rational Procedure for the Preliminary Design of Minimum Volume Gears

AGMA 901-A92

Manufacturers Association **CAUTION NOTICE**: AGMA technical publications are subject to constant improvement, revision or withdrawal as dictated by experience. Any person who refers to any AGMA Technical Publication should be sure that the publication is the latest available from the Association on the subject matter.

[Tables or other self-supporting sections may be referenced. Citations should read: See AGMA 901-A92, *A Rational Procedure for the Preliminary Design of Minimum Volume Gears*, published by the American Gear Manufacturers Association, 1001 N. Fairfax Street, Suite 500, Alexandria, Virginia 22314, http://www.agma.org.]

Approved May 1992

ABSTRACT

A simple, closed-form procedure is presented as a first step in the design of minimum volume spur and helical gearsets. The procedure includes methods for selecting geometry and dimensions, considering maximum pitting resistance, bending strength, and scuffing resistance. It also includes methods for selecting profile shift.

Published by

American Gear Manufacturers Association 1001 N. Fairfax Street, Suite 500, Alexandria, Virginia 22314

Copyright © 1992 by American Gear Manufacturers Association Reaffirmed November 1997 Reformatted May 2013 All rights reserved.

No part of this publication may be reproduced in any form, in an electronic retrieval system or otherwise, without prior written permission of the publisher.

Printed in the United States of America

ISBN: 1-55589-579-4

Contents

Foreword					
	1.1 1.2	Procedure			
^		·			
2		itions and symbols			
	2.1 2.2	Definitions			
3		variables			
J	•	Materials and heat treatment			
	3.1				
	3.1.1 3.1.2 3.1.3 3.1.4	Surface hardeningThrough hardening			
		Allowable stress numbers	4		
	3.2	Design life			
	3.3 3.4 3.5	Aspect ratio			
		Combined derating factors, C_d and K_d			
	3.5.1	Application factor, C_a and K_a	6		
	3.5.2	Load distribution factor, C_m and K_m	7		
	3.5.3 3.5.4				
		N. C.			
	3.6 3.7	Geometry factors, <i>I</i> and <i>J</i>			
	3.7.1	Minimum volume gearsets			
	3.7.1				
	3.8	Cutter profile angle	10		
	3.9	Tool selection	11		
	3.10 3.11	Selecting a helix angle			
4		•			
4 5		erred number of pinion teethgn algorithm			
6	Desi	gn audit	16		
7	Cons	iderations for improved rating	16		
	7.1	Improve bending fatigue resistance with:			
-	7.2 7.3	Improve pitting fatigue resistance with: Improve scuffing resistance with:			
	7.4	Profile shift (addendum modification)	17		
	7.5	Summary	18		
A	nnexes				
Annex A (informative) Profile shift (addendum modification)					
Annex B (informative) Ratio split for minimum volume					
Annex D (informative) Example problems					
Annex E References and bibliography					
Ta	ables				
Τá	Table 1 - Symbols used in equations2				
Ta	Table 1 - Symbols used in equations				
16	able 3 - Allowable bending stress numbers for steel gears'				

This is a preview of "AGMA 901-A92 (R2015)". Click here to purchase the full version from the ANSI store.

Table 4 - Typical application factors*, C_a and K_a	6
Table 5 - Typical load distribution factors	
Table 6 - Effects of helix angle in parallel shaft gearing	
Figures	
Figure 1 - Two branch double stage gearing	7
Figure 2 - Preferred number of pinion teeth	13
Figure 3 - Preferred number of pinion teeth for spur gear (unmodified)	13
Figure 4 - Preferred number of pinion teeth for spur gear (modified)	
Figure 5 - Preferred number of pinion teeth for spur gear where redesign should be considered	

Foreword

[The foreword, footnotes and annexes, if any, in this document are provided for informational purposes only and are not to be construed as a part of AGMA 901-A92, *A Rational Procedure for the Preliminary Design of Minimum Volume Gears.*]

Gear design is a process of synthesis where gear geometry, materials, heat treatment, manufacturing methods, and lubrication are selected to meet the performance requirements of a given application. The designer must design the gearset with adequate pitting resistance, bending strength, and scuffing resistance to transmit the required power for the design life. With the algorithm presented here, one can select materials and heat treatment within the economic constraints and limitations of manufacturing facilities, and select the gear geometry to satisfy constraints on weight, size and configuration. The gear designer can minimize noise level and operating temperature by minimizing the pitchline velocity and sliding velocity. This is done by specifying high gear accuracy and selecting material strengths consistent with maximum material hardness, to obtain minimum volume gearsets with teeth no larger than necessary to balance the pitting resistance and bending strength.

Gear design is not the same as gear analysis. Existing gearsets can only be analyzed, not designed. While design is more challenging than analysis, current textbooks do not provide procedures for designing minimum volume gears. They usually recommend that the number of teeth in the pinion be chosen based solely on avoiding undercut. This information sheet, based on the work of R. Errichello [1], will show why this practice, or any procedure which arbitrarily selects the number of pinion teeth, will not necessarily result in minimum volume gearsets. Although there have been many technical papers on gear design (for example [2] and [3]), most advocate using computer-based search algorithms which are unnecessary. Tucker [4] came the closest to an efficient algorithm, but he did not show how to find the preferred number of teeth for the pinion.

This information sheet includes the design of spur and helical gears. Other gear types could be designed by a similar algorithm with some slight modifications to the one presented here.

AGMA 901-A92 was approved by the Helical Gear Rating Committee in March, 1992 and approved by the AGMA Board of Directors as of May, 1992.

Suggestions for improvement of this standard will be welcome. They should be sent to the American Gear Manufacturers Association, 1001 N. Fairfax Street, Suite 500, Alexandria, Virginia 22314.

PERSONNEL of the AGMA Helical Gear Rating Committee

ACTIVE MEMBERS

.The Gear Works-Seattle
.Falk
.Peerless-Winsmith
.C&M of Indiana
.General Motors/Allison
Bodensieck Engineering
Metal Improvement Company
.General Electric
Terrell Gear Drives
.Bison Gear
.Boeing
.Geartech
.Cincinnati Gear
Emerson Power Transmission
.Cincinnati Gear
.Amarillo Gear Co.
Lufkin Industries
.Gear Engineers, Inc
.Milburn Engineering
The Timken Co.
Pratt & Whitney
.WesTech Gear Corp.
.Philadelphia Gear
.Academic Member
Sewall Gear
.Reliance Electric/Reeves
.Mobile Pulley & Mach. Works
Sewall Gear
.3E Software & Engrg. Cons.
.Arrow Gear
Academic Member

AGMA 901-A92

American Gear Manufacturers Association -

A Rational Procedure for the Preliminary Design of Minimum Volume Gears

1 Scope

This information sheet is intended for the student or beginning gear designer, to provide an outline of a preliminary design procedure which will lead to a rational design for spur and helical gear pairs within constraints such as:

- required gear ratio;
- required torque capacity;
- specified center distance;
- material selection.

This method could be extended to other gear types given the appropriate constants and factors.

1.1 Procedure

The simple closed form of the procedure allows the designer to explore options with a minimum of computation so that the important design decisions regarding loads, overloads, material, and tooling selections are not obscured by the need to spend a long time calculating each possibility.

This information sheet will demonstrate to the user that the traditional beginning point for gear design, selecting the minimum number of pinion teeth to avoid undercut, will rarely lead to the best design.

As this procedure is approximate, it is necessary to audit the design (see clause 6).

1.2 Exceptions

The procedure described herein incorporates major design considerations and leads toward minimum volume gear designs based upon the criteria chosen. For the final gear design, additional influencing factors beyond those in this information sheet include shaft deflection limits, sound level, cost, etc. Any of these could influence the design of the gear envelope and final volume.

It is not the intent of this information sheet to include the calculation of the profile shift coefficient (addendum modification coefficient). It is, however, necessary to inform the reader that profile shift exists, how it can affect gear design, and where it comes into play in designing a gearset. Some of the important factors relating to profile shift are discussed in 7.4.

Overhung pinions or gears are not covered by this information sheet because of the difficulty in determining an accurate value for the load distribution factor.

2 Definitions and symbols

2.1 Definitions

The terms used, wherever applicable, conform to the following standards:

ANSI Y10.3-1968, Letter Symbols for Quantities Used in Mechanics of Solids ANSI/AGMA 1012-F90, Gear Nomenclature, Definitions of Terms with Symbols AGMA 904-B89, Metric Usage