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# **Eurocode 2: Betonkonstruktioner – Del 1-2: Generelle regler – Brandteknisk dimensionering**

Eurocode 2: Design of concrete structures –  
Part 1-2: General rules – Structural fire design

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**IDT med: EN 1992-1-2:2004/A1:2019**

**DS-publikationen er på engelsk.**

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## EUROPÄISCHE NORM

May 2019

ICS 91.010.30; 91.080.40

English Version

## Eurocode 2: Design of concrete structures - Part 1-2: General rules - Structural fire design

Eurocode 2 : Calcul des structures en  
béton - Partie 1-2 : Règles générales -  
Calcul du comportement au feu

Eurocode 2: Bemessung und Konstruktion  
von Stahlbeton- und Spannbetontragwerken  
- Teil 1-2: Allgemeine Regeln -  
Tragwerksbemessung für den Brandfall

This amendment A1 modifies the European Standard EN 1992-1-2:2004; it was approved by CEN on 8 March 2019.

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## Contents

Page

European foreword .....	3
1 <b>Modification of 4.2.1(1)</b> .....	4
2 <b>Modification of 5.3.3(1)</b> .....	4
3 <b>New Annex C</b> .....	4
<b>Annex C (informative) Buckling of columns under fire conditions</b> .....	5

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## European foreword

This document ([EN 1992-1-2:2004/A1:2019](#)) has been prepared by Technical Committee CEN/TC 250 "Structural Eurocodes", the secretariat of which is held by BSI.

This European Standard shall be given the status of a national standard, either by publication of an identical text or by endorsement, at the latest by November 2019, and conflicting national standards shall be withdrawn at the latest by November 2019.

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## **Eurocode 2: Design of concrete structures –**

### **Part 1-2: General rules – Structural fire design**

#### **1 Modification of 4.2.1(1)**

*Replace existing NOTE 2 in paragraph (1) of 4.2.1 with the following new NOTE 2:*

"NOTE 2 Tabulated data for the fire design of slender reinforced columns in braced and unbraced systems is given in [Annex C](#)".

#### **2 Modification of 5.3.3(1)**

*Delete the following sentence in paragraph (1) of 5.3.3:*

"Further information is given in [Annex C](#)".

#### **3 New [Annex C](#)**

*Replace the existing [Annex C](#) with the following:*

"

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## Annex C (informative)

### Buckling of columns under fire conditions

(1) The tables in this annex provide information for assessing columns with rectangular cross section in braced or unbraced structures giving the maximum permissible slenderness ratio under fire conditions,  $\lambda_{fi,max}$ . The slenderness ratio in the fire situation is  $\lambda_{fi} = l_{0,fi} / i$ , where the effective column length,  $l_{0,fi}$ , is defined by the actual length of the column,  $l$ , and the support conditions under fire conditions.

The effective length in fire  $l_{0,fi}$  may be taken as the effective length  $l_0$  in ambient conditions in all cases. For braced building structures where the required standard fire exposure is higher than 30 min and the column is continuous through a slab that provides fire separation, the effective length  $l_{0,fi}$  may be taken as  $0,5 l$  for intermediate floors and  $0,5 l \leq l_{0,fi} \leq 0,7 l$  for the upper floor. Intermediate values of  $l_{0,fi} / l$  may be chosen depending of the actual moment restraints at the supports under fire conditions. For unbraced structures  $l_{0,fi}$  should be taken as the lesser of  $2l$  or  $l_0$  in ambient conditions.

The radius of gyration  $i$  is shown in Figure C.1.

The tables are valid for the range of thermal conductivity between the lower and upper limit given in 3.3.3. The column slenderness  $\lambda_{fi}$  is limited to values  $\leq 55$ .

(2) The following parameters are needed to use the tables in this annex:

$h, b$  dimensions of column cross section,  $b \leq h$

$A_c$  cross sectional area of column,  $A_c = b \times h$

$n_{fi}$

$$\text{load ratio: } n_{fi} = \frac{N_{Ed,fi}}{\left( \frac{A_c \times f_{cd}}{\alpha_{cc}} \right) + 2 \times \text{Min}(A_{sc,e}; A_{st,e}) \times f_{yd}} \quad (\text{C.1})$$

$\eta$

$$\eta = \frac{2 \times \text{Min}(A_{sc,e}; A_{st,e}) \times f_{yd}}{\frac{A_c \times f_{cd}}{\alpha_{cc}}}$$

modified mechanical reinforcement ratio:  $\eta =$

$A_{sc,e}$  and  $A_{st,e}$  are defined in (3).

$e_N$  modified, total first order eccentricity of the normal force,  $N_{Ed,fi}$ ,

see Figure C.1. However,  $e_N \geq e_0$ , see [EN 1992-1-1:2004](#), 6.1(4)

$a$  axis distance of the main bars

$N_{Ed,fi}$  design axial load in the fire condition

$M_{0Ed,fi}$  design first order moment in the fire condition

The tables are not applicable for  $f_{ck} > 50$  MPa. The reference dimension for the cross section in the tables is always the smaller cross section dimension  $b$ .

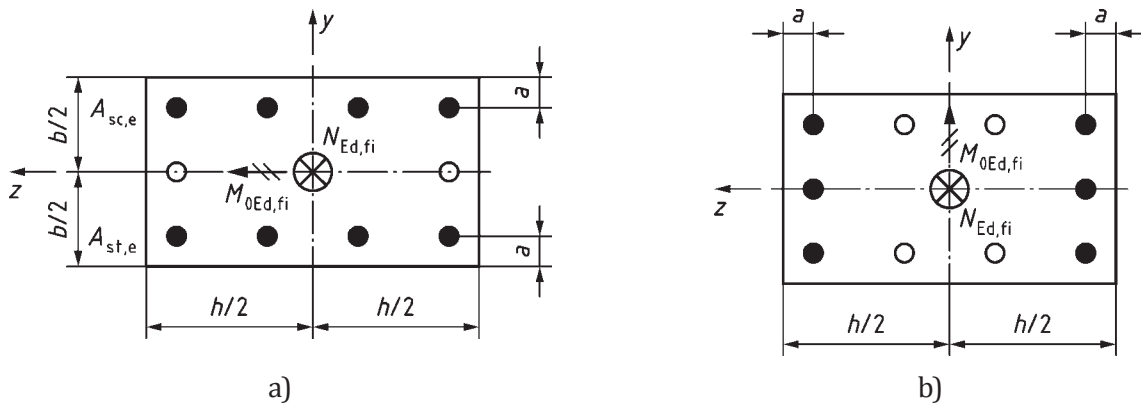
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(3)  $A_{sc,e}$  is the cross-sectional area of the reinforcement at the distance  $a$  from the most compressed side of the column and  $A_{st,e}$  is the cross-sectional area of the reinforcement at the distance  $a$  from the least compressed side of the column. Other reinforcing bars in the cross section are disregarded.

Buckling around  $y$ -axis and  $z$ -axis should be examined. The tables may be used for buckling around both the  $z$ -axis and the  $y$ -axis as defined in Figure C.1. They may also be used for rectangular cross sections with asymmetric reinforcement arrangement. For buckling around both the  $z$ -axis or the  $y$ -axis, the smaller dimension  $b$  should be used as the parameter in the tables.

For buckling around the  $y$ -axis, the actual first order eccentricity of the normal force in the fire condition may be reduced by the factor  $b/h$ . Using the tables,  $e_N$  always is at least 20 mm.

For columns with asymmetric reinforcement arrangements, the minimum values of  $A_{sc,e}$  and  $A_{st,e}$  shall be used.



Buckling around  $z$ -axis:

Buckling around  $y$ -axis:

$$e_N = \frac{M_{0Ed,fi}}{N_{NEd,fi}} ;$$

$$i = \frac{b}{\sqrt{12}}$$

$$e_N = \frac{b}{h} \times \frac{M_{0Ed,fi}}{N_{NEd,fi}} \geq 0,5 \frac{M_{0Ed,fi}}{N_{NEd,fi}}$$

$$i = \frac{h}{\sqrt{12}}$$

**Key**

- reinforcing bars to be disregarded
- reinforcing bars

**Figure C.1 — Rectangular cross sections**

(4) For rectangular cross sections the minimum number of reinforcing bars in each  $A_{sc}$  and  $A_{st}$  is given in Table C.1.

**Table C.1 — Minimum number of reinforcing bars**

$\omega$	Minimum dimension of column section, $b$					
	600 mm	500 mm	400 mm	300 mm	250 mm	200 mm
0,1	3	3	3	2	2	2
0,2	3	3	3	2	2	2
0,5	3	3	3	2	2	2
1,0	5	4	3	2	2	2

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(5) In accordance with [EN 1992-1-1:2004](#), 4.4.1.2(3) the axis distance for the reinforcing bars in the cross section shall fulfil  $a \geq 1,5\phi_{sl}$ , where  $\phi_{sl}$  is the bar diameter.

(6) When using the tables within this annex, linear interpolation is permitted.

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Table C.2 — Maximum permissible slenderness ratio under fire conditions for braced and unbraced columns: R30

R30	$b$ (mm)		600			500			400			300			250			200		
	$e_N$ (mm)	$a$ (mm)	$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$		
			0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6
$\omega = 0,1$	20	25	55	55	52	55	55	50	55	47	55	50	40	55	47	35	55	42	28	
	20	45	55	55	55	55	55	55	55	55	55	55	49	55	55	44	55	49	36	
	20	65	55	55	55	55	55	55	55	55	55	55	55	55	55	48	55	46	37	
	20	85	55	55	55	55	55	55	55	55	55	55	55	55	54	47	54	44		
	50	25	55	55	46	55	54	42	55	36	54	39	21	49	32		40	18		
	50	45	55	55	55	55	55	52	55	45	55	47	27	55	38		47	19		
	50	65	55	55	55	55	55	55	55	51	55	51	31	55	38		43			
	50	85	55	55	55	55	55	55	55	55	55	47	28	52	33		37			
	100	25	55	48	32	55	42	22	52	33	35			21						
	100	45	55	55	41	55	51	29	55	40	45			30						
	100	65	55	55	47	55	55	33	55	43				28						
	100	85	55	55	55	55	55	32	55	39				22						

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Table C.2 (continued)

R30	b (mm)		600			500			400			300			250			200					
	e <sub>N</sub> (mm)	n <sub>fi</sub>	λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>					
			0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6			
	20	25	55	55	54	55	55	52	55	55	48	55	55	53	40	55	55	50	36	55	55	44	28
	20	45	55	55	55	55	55	55	55	55	55	55	55	55	51	55	55	55	45	55	55	51	36
	20	65	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	48	55	55	47	36
	20	85	55	55	55	55	55	55	55	55	55	55	55	55	54	55	55	54	45	55	55	42	34
	50	25	55	55	47	55	55	43	55	54	37	55	55	43	21	55	55	36		50	50	22	
	50	45	55	55	55	55	55	55	55	55	47	55	55	52	29	55	55	43		55	55	24	
	50	65	55	55	55	55	55	55	55	55	54	55	55	55	32	55	55	40		48			
	50	85	55	55	55	55	55	55	55	55	51	55	55	47	26	55	55	31		38			
	100	25	55	55	33	55	55	24	55	38		48				37							
	100	45	55	55	44	55	55	33	55	47		55	55	18		48				23			
	100	65	55	55	51	55	55	38	55	51		55	55			45							
	100	85	55	55		55	55	35	55	43		52				28							

ω = 0,2

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Table C.2 (continued)

R30	b (mm)		600			500			400			300			250			200		
	e <sub>N</sub> (mm)	a (mm)	λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>					
			0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6			
ω = 0,5	20	25	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	
	20	45	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	
	20	65	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	
	20	85	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	
	50	25	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	
	50	45	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	
	50	65	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	
	50	85	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	
	100	25	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	
	100	45	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	
100	65	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55		
100	85	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55		



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Table C.3 — Maximum permissible slenderness ratio under fire conditions for braced and unbraced columns: R60

R60	$b$ (mm)		600			500			400			300			250			200		
	$e_N$ (mm)	$\alpha$ (mm)	$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$		
			0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6
$\omega = 0,1$	20	25	55	48	39	55	46	36	52	43	31	43	35	21	38	30	31	20	31	20
	20	45	55	55	48	55	55	45	55	51	39	55	42	29	49	36	22	40	25	25
	20	65	55	55	55	55	55	52	55	55	46	55	47	36	51	39	27	38	25	25
	20	85	55	55	55	55	55	55	55	55	50	55	47	38	48	37	29	33	24	24
	50	25	52	43	32	50	40	27	45	34	16	33	20		25					
	50	45	55	53	40	55	49	35	55	42	24	46	28		38	15		24		
	50	65	55	55	47	55	55	41	55	48	29	51	32		40	15		23		
	50	85	55	55	54	55	55	47	55	49	32	49	31		36					
	100	25	45	34	15	40	27		31	10										
	100	45	55	43	23	54	36		45	20		26								
	100	65	55	49	28	55	41		51	23		30								
	100	85	55	54	32	55	44		52	22		28								

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Table C.3 (continued)

R60	$b$ (mm)		600			500			400			300			250			200		
	$n_{fi}$	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	
			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$					
$e_N$ (mm)	$a$ (mm)																			
20	25	55	49	38	55	47	35	55	43	30	44	34	19	40	29		33	18		
20	45	55	55	49	55	55	46	55	54	40	55	44	30	55	38	22	45	26		
20	65	55	55	55	55	55	54	55	55	48	55	50	36	55	40	26	42	25		
20	85	55	55	55	55	55	55	55	55	51	55	48	37	51	37	27	33	21		
50	25	55	44	31	54	41	25	50	35	14	35	19		28						
50	45	55	55	42	55	53	36	55	46	26	54	31		46	18		33			
50	65	55	55	50	55	55	43	55	52	31	55	35		48	18		29			
50	85	55	55	55	55	55	49	55	53	34	55	32		41						
100	25	50	35	11	45	28		38	11											
100	45	55	48	25	55	40		55	26		38			23						
100	65	55	55	31	55	46	10	55	30		43			25						
100	85	55	55	36	55	50	12	55	29		39									

$\omega = 0,2$

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Table C.3 (continued)

R60	b (mm)		600			500			400			300			250			200		
	e <sub>N</sub> (mm)	a (mm)	λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>		
			0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6
	20	25	55	50	35	55	47	31	55	43	26	48	30	43	24	36				
	20	45	55	55	51	55	55	47	55	55	42	55	47	55	40	54	21	54	28	
	20	65	55	55	55	55	55	55	55	55	50	55	54	55	43	47	26	47	26	
	20	85	55	55	55	55	55	55	55	55	53	55	51	55	38	34	24	34	18	
	50	25	55	45	26	55	41	19	55	34		39		33		20				
	50	45	55	55	43	55	55	38	55	51	27	55	35	55	23	44				
	50	65	55	55	53	55	55	47	55	55	35	55	40	55	23	36				
	50	85	55	55	55	55	55	53	55	55	37	55	36	48	14					
	100	25	55	35		55	27		49			18								
	100	45	55	54	27	55	47	9	55	34		55		43						
	100	65	55	55	37	55	55	20	55	40		55		41						
	100	85	55	55	43	55	55	23	55	40		53		25						

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Table C.3 (continued)

R60	$b$ (mm)		600			500			400			300			250			200			
	$n_{fi}$	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6		
			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$						
	$e_N$ (mm)	$a$ (mm)																			
	20	25	55	55	36	55	50	30	18	40	18	48	22	43	14	35	35	35	30		
	20	45	55	55	55	55	55	50	42	55	42	55	50	55	42	55	55	42	19	30	
	20	65	55	55	55	55	55	55	52	55	52	55	55	55	45	52	55	45	26	27	
	20	85	55	55	55	55	55	55	55	55	55	55	54	55	39	34	55	39	22	34	
	50	25	55	55	27	55	43	15	30	30	30	39		32		18					
	50	45	55	55	48	55	55	41	28	55	28	55	38	55	25	49					
	50	65	55	55	55	55	55	51	38	55	38	55	44	55	28	41					
	50	85	55	55	55	55	55	55	40	55	40	55	40	53	17						
	100	25	55	55	41	55	29			54		18									
	100	45	55	55	32	55	55	14	39	55	39	55		51		27					
	100	65	55	55	44	55	55	27	48	55	48	55		51							
	100	85	55	55	50	55	55	31	48	55	48	55		34							

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Table C.4 — Maximum permissible slenderness ratio under fire conditions for braced and unbraced columns: R90

R90	$b$ (mm)		600			500			400			300			250			200		
	$e_N$ (mm)	$\alpha$ (mm)	$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$		
			0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6
$\omega = 0,1$	20	25	49	42	33	47	40	29	44	36	23	34	26	29	18	21				
	20	45	55	49	39	55	46	35	53	41	29	41	30	16	35	22				
	20	65	55	55	46	55	53	42	55	47	35	48	35	22	40	25				
	20	85	55	55	52	55	55	47	55	51	40	48	36	25	37	25	14			
	50	25	45	37	25	42	33	19	37	26		24								
	50	45	55	44	31	52	40	24	46	32	9	32	13		23					
	50	65	55	51	37	55	46	30	54	37	15	39	18		28					
	50	85	55	55	43	55	50	35	55	40	19	39	17		26					
	100	25	38	27		32	19		23											
	100	45	48	34	9	42	25		33											
	100	65	55	40	16	51	31		41			16								
	100	85	55	44	19	55	34		43			16								

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Table C.4 (continued)

R90	b (mm)		600			500			400			300			250			200		
	e <sub>N</sub> (mm)	n <sub>fi</sub>	λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>					
			0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6			
	20	25	52	42	31	40	27	46	35	21	35	24	30	16	21					
	20	45	55	51	39	48	35	55	43	29	45	31	15	22	27					
	20	65	55	55	47	55	43	55	50	36	54	36	22	26	28					
	20	85	55	55	54	55	49	55	53	40	53	37	24	25	22					
	50	25	48	37	23	33	16	40	26		25		15							
	50	45	55	46	31	41	24	53	34		37	13	28							
	50	65	55	55	39	49	31	55	40	17	46	20	35							
	50	85	55	55	45	54	36	55	43	21	45	19	30							
	100	25	41	27		36	18	27												
	100	45	55	36	8	50	27	42			17									
	100	65	55	45	19	55	35	52	14		30									
	100	85	55	50	23	55	39	54	13		28									

ω = 0,2

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Table C.4 (continued)

R90	b (mm)		600			500			400			300			250			200		
	e <sub>N</sub> (mm)	a (mm)	λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>		
			0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6
	20	25	55	41	26	54	38	22	51	33	15	36	18	31		20				
	20	45	55	53	38	55	50	34	55	44	27	51	30	44	20	29				
	20	65	55	55	49	55	55	44	55	54	37	55	39	51	28	32				
	20	85	55	55	55	55	55	51	55	55	42	55	39	45	25	22				
	50	25	53	35	16	50	31		46	22		27		18						
	50	45	55	48	30	55	44	22	55	35		44		35						
	50	65	55	55	41	55	55	34	55	45	20	55	24	43						
	50	85	55	55	48	55	55	40	55	48	23	54	23	36						
	100	25	47	24		42	11		35											
	100	45	55	39		55	30		55			30								
	100	65	55	52	22	55	42		55	25		44		24						
	100	85	55	55	29	55	47		55	26		40								

ω = 0,5

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Table C.4 (continued)

R90	b (mm)		600			500			400			300			250			200		
	e <sub>N</sub> (mm)	n <sub>fi</sub>	λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>		
			0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6
	20	25	55	42	23	55	37	16	52	27	35		29							
	20	45	55	55	41	55	55	35	55	45	54	27	46	17						30
	20	65	55	55	54	55	55	48	55	55	55	41	55	30						35
	20	85	55	55	55	55	55	55	55	55	55	41	48	26						23
	50	25	55	37	8	55	29		47	12	25									
	50	45	55	55	33	55	48	22	55	35	47		37							
	50	65	55	55	46	55	55	37	55	50	55	28	49							22
	50	85	55	55	54	55	55	44	55	53	55	27	40							
	100	25	55	24		51			36											
	100	45	55	47		55	35		55		33									
	100	65	55	55	29	55	50		55	31	52									32
	100	85	55	55	36	55	55	10	55	34	48		20							

ω = 1,0

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Table C.5 — Maximum permissible slenderness ratio under fire conditions for braced and unbraced columns: R120

R120	$b$ (mm)		600			500			400			300			250			200		
	$e_N$ (mm)	$\alpha$ (mm)	$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$		
			0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6
$\omega = 0,1$	20	25	45	38	29	43	36	24	39	31	17	29	19	23						
	20	45	52	44	33	50	40	29	45	35	21	32	21	26						
	20	65	55	50	39	55	46	35	53	40	27	39	25	30						
	20	85	55	55	45	55	51	40	55	44	32	40	27	15	29	14				
	50	25	41	34	21	38	29	12	32	20		17								
	50	45	48	38	25	45	33	16	38	24		21								
	50	65	55	45	31	54	39	22	46	29		30		18						
	50	85	55	50	35	55	43	27	50	32		31		15						
	100	25	33	23		27	12		15											
	100	45	41	28		35	17		24											
100	65	51	34		44	23		33												
100	85	55	38	6	49	26		37												

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Table C.5 (continued)

R120	$b$ (mm)		600			500			400			300			250			200		
	$n_{fi}$	$a$ (mm)	$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$		
			0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6
	20	25	47	38	27	44	35	22	41	30	14	29	16	23						
	20	45	55	44	32	53	41	28	49	35	20	33	19	27						
	20	65	55	53	40	55	49	35	55	42	27	44	26	33						
	20	85	55	55	46	55	54	41	55	46	32	44	27	31						
	50	25	43	33	18	39	28		34	19		18								
	50	45	53	39	23	49	34	14	43	24		23								
	50	65	55	48	32	55	42	23	54	32		36		23						
	50	85	55	53	37	55	46	28	55	35		36		19						
	100	25	35	22		30	8		19											
	100	45	46	28		40	17		30											
	100	65	55	37		54	27		43			17								
	100	85	55	42	11	55	30		47			17								

$\omega = 0,2$

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Table C.5 (continued)

R120	b (mm)		600			500			400			300			250			200		
	e <sub>N</sub> (mm)	a (mm)	λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>		
			0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6
	20	25	49	35	20	47	31	15	43	25	30	23								
	20	45	55	44	29	55	40	24	55	34	36	27								
	20	65	55	55	41	55	52	36	55	45	51	38								
	20	85	55	55	48	55	55	42	55	49	50	34								
	50	25	46	29		43	23		38	10	20									
	50	45	55	39	18	55	33		50	22	27									
	50	65	55	52	32	55	46	24	55	36	44	29								
	50	85	55	55	39	55	52	30	55	40	44	24								
	100	25	39	15		34			25											
	100	45	54	27		49	13		40											
	100	65	55	42	6	55	32		55		31									
	100	85	55	49	17	55	38		55	11	29									

ω = 0,5

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Table C.5 (continued)

R120	$b$ (mm)		600			500			400			300			250			200		
	$e_N$ (mm)	$n_{fi}$	$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$		
			0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6
	20	25	55	33	12	27	43	17	28	17	28	17	28	17	28	17	28	17	28	17
	20	45	55	50	30	43	55	31	34	31	34	31	34	31	34	31	34	31	34	31
	20	65	55	55	45	55	55	47	55	47	55	47	55	47	55	47	55	47	55	47
	20	85	55	55	53	55	55	53	55	53	55	53	55	53	55	53	55	53	55	53
	50	25	52	25	25	16	36	36	15	36	15	36	15	36	15	36	15	36	15	36
	50	45	55	44	19	35	52	17	24	17	24	17	24	17	24	17	24	17	24	17
	50	65	55	55	36	51	55	38	49	38	49	38	49	38	49	38	49	38	49	38
	50	85	55	55	44	55	55	44	49	44	49	44	49	44	49	44	49	44	49	44
	100	25	46			37	22				22					22				
	100	45	55	33		16	42				42					42				
	100	65	55	51	13	39	55	14	37	14	37	14	37	14	37	14	37	14	37	14
	100	85	55	55	24	46	55	22	36	22	36	22	36	22	36	22	36	22	36	22

$\omega = 1,0$

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Table C.6 — Maximum permissible slenderness ratio under fire conditions for braced and unbraced columns: R180

R180	<i>b</i> (mm)		600			500			400			300			250			200		
	<i>e<sub>N</sub></i> (mm)	<i>a</i> (mm)	$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$		
			0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6
$\omega = 0,1$	20	25	40	34	22	37	30	17	31	22										
	20	45	45	37	26	42	33	20	35	24										
	20	65	51	41	30	47	37	25	39	27	12									
	20	85	55	46	35	53	41	29	44	30	17									
	50	25	36	28	13	32	22		23											
	50	45	41	32	16	37	25		28	10										
	50	65	47	36	21	42	29	7	33	14										
	50	85	54	40	25	48	33	13	37	17										
	100	25	27	16		20														
	100	45	33	20		26														
100	65	40	23		32			17												
100	85	47	28		39	11		23												

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Table C.6 (continued)

R180	$b$ (mm)		600			500			400			300			250			200		
	$e_N$ (mm)	$n_{fi}$	$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$		
			0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6
	20	25	40	32	20	28	13	31	19	21										
	20	45	48	37	24	32	18	37	23	23										
	20	65	55	42	30	37	24	43	27	26										
	20	85	55	48	35	43	29	49	31	29										
	50	25	36	27	6	20		24												
	50	45	44	31	14	25		31												
	50	65	52	36	19	29		37	14	14										
	50	85	55	43	26	35	14	43	19	19										
	100	25	28	13		21														
	100	45	37	19		30		15												
	100	65	45	24		39		25												
	100	85	55	31		47	16	32												

$\omega = 0,2$

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Table C.6 (continued)

R180	b (mm)		600			500			400			300			250			200		
	e <sub>N</sub> (mm)	a (mm)	λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>		
			0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6
	20	25	41	28	11	38	22		32	11		19								
	20	45	53	35	19	49	30	12	41	19		21								
	20	65	55	43	27	55	37	21	49	27		26								
	20	85	55	52	36	55	46	29	55	34	15	33								
	50	25	37	20		33	10		25											
	50	45	49	29		45	21		35											
	50	65	55	37	15	55	29		44	12		14								
	50	85	55	46	26	55	39	14	52	23		25								
	100	25	29			23														
	100	45	43	12		37			23											
	100	65	55	24		48			34											
	100	85	55	36		55	22		43											

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Table C.6 (continued)

R180	b (mm)		600			500			400			300			250			200		
	e <sub>N</sub> (mm)	n <sub>fi</sub>	λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>		
			0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6
	a (mm)																			
	20	25	42	20	38	13	30													
	20	45	55	36	53	28	40	14												
	20	65	55	48	55	40	52	25												
	20	85	55	55	55	50	55	36	14	36	15									
	50	25	38	6	32		22													
	50	45	55	29	49	17	34													
	50	65	55	42	55	32	47													
	50	85	55	53	55	43	55	26	29	29										
	100	25	30		20															
	100	45	52	11	41		21													
	100	65	55	31	55	9	37													
	100	85	55	43	55	29	50													

ω = 1,0

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Table C.7 — Maximum permissible slenderness ratio under fire conditions for braced and unbraced columns: R240

R240	<i>b</i> (mm)		600			500			400			300			250			200		
	<i>e<sub>N</sub></i> (mm)	<i>a</i> (mm)	$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$		
			0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6
	20	25	37	30	18	33	25	9	25	11										
	20	45	41	33	21	36	27	12	28	13										
	20	65	45	36	24	39	29	16	31	16										
	20	85	50	39	28	44	32	20	34	19	12									
	50	25	33	24		27	16		17											
	50	45	36	27	8	30	18		20											
	50	65	41	30	12	34	21		23											
	50	85	46	33	17	39	24		28											
	100	25	24	10		14														
	100	45	28	12		18														
	100	65	33	15		23														
	100	85	39	19		29			10											

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Table C.7 (continued)

R240	b (mm)		600			500			400			300			250			200		
	e <sub>N</sub> (mm)	a (mm)	λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>		
			0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6
	20	25	37	29	15	33	23	26												
	20	45	42	32	19	37	25	29	10											
	20	65	48	35	22	42	29	33	14											
	20	85	55	40	28	48	33	37	19	12										
	50	25	33	22		27	13	17												
	50	45	38	26		32	16	21												
	50	65	44	29	9	37	20	26												
	50	85	52	34	16	44	24	31												
	100	25	25			15														
	100	45	31	9		21														
	100	65	37	14		28														
	100	85	45	20		35		18												

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Table C.7 (continued)

R240	b (mm)		600			500			400			300			250			200		
	e <sub>N</sub> (mm)	a (mm)	λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>			λ <sub>fi,max</sub>		
			0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6
	20	25	38	23		33	16													
	20	45	45	28	11	39	21													
	20	65	53	34	18	47	26		9											
	20	85	55	41	26	55	34	16	19											
	50	25	34	14		28														
	50	45	41	21		35														
	50	65	50	27		43	16													
	50	85	55	35	13	51	25													
	100	25	26			16														
	100	45	34			26														
	100	65	44	7		35														
	100	85	54	22		44														

ω = 0,5

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Table C.7 (continued)

R240	$b$ (mm)		600			500			400			300			250			200		
	$e_N$ (mm)	$n_{fi}$	$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$			$\lambda_{fi,max}$		
			0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6	0,2	0,4	0,6
	$a$ (mm)																			
	20	25	37	14		32			21											
	20	45	48	24		40	13		26											
	20	65	55	37	15	53	26		35											
	20	85	55	47	27	55	36	15	45	19										
	50	25	33			26														
	50	45	44	14		35			17											
	50	65	55	30		48	15		28											
	50	85	55	41	14	55	28		40											
	100	25	24			11														
	100	45	37			24														
	100	65	54	12		41			9											
	100	85	55	29		53			29											

$\omega = 1,0$

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